

ASME BPVC VIII-1 2019

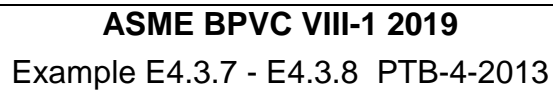
Example E4.3.7 - E4.3.8 PTB-4-2013

Table of contents

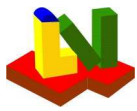
Table of contents	1
Summary	2
E4.3.7 Large End - Cone-to-cylinder junction at large end under internal pressure - ASME BPVC VIII-1 UG-32 & Appendix-1: 2019	3
E4.3.7 Small End - Cone-to-cylinder junction at small end under internal pressure - ASME BPVC VIII-1 UG-32 & Appendix-1: 2019	5
E4.3.8 - Cone with knuckle under internal pressure - ASME BPVC VIII-1 UG-32 & Appendix-1: 2019	7
Appendix: Material documentation	9

Layout

Input values:	1.234	or	1.234
Calculated values:	1.234	or	1.234
Critical values:	1.234	or	1.234
Estimated values:	1.234	or	1.234



Strength Calculation Software			Program System ATLAS		Version		8.32.1					
Developed by Lauterbach Verfahrenstechnik GmbH												
Certified per DIN EN ISO 9001:2015			Certificate Number 01 100 044763									
					LV Soft				ASME		Diff [%]	
Example E4.3.7 - Conical transition Without a knuckle (large End)												
			Required cylinder thickness t		37,48	mm	1,48	in	1,48	in	0,08%	
			Required cone thickness tr		39,93	mm	1,57	in	1,57	in	0,08%	
Example E4.3.7 - Conical transition Without a knuckle (Smal End)								in				
			Required cylinder thickness t		23,78	mm	0,94	in	0,94	in	0,07%	
			Required cone thickness tr		25,25	mm	0,99	in	0,99	in	0,07%	
			Required area Ars		2.087,34	mm ²	3,24	in ²	3,24	in ²	0,03%	
			Required area Aes		4.054,38	mm ²	6,28	in ²	6,28	in ²	0,11%	
Example E4.3.8 - Conical transition With a knuckle												
			Required knuckle thickness t		17,20	mm	0,68	in	0,68	in	0,07%	
			Required cone thickness tr		24,74	mm	0,97	in	0,97	in	0,08%	



E4.3.7 Large End - Cone-to-cylinder junction at large end under internal pressure - ASME BPVC VIII-1 UG-32 & Appendix-1: 2019

Cone-to-cylinder junction (wide end)

Type of reinforcing ring

(0 = no, 1 = at the cylinder, 2 = at the cone)

Without stiffener

Design pressure

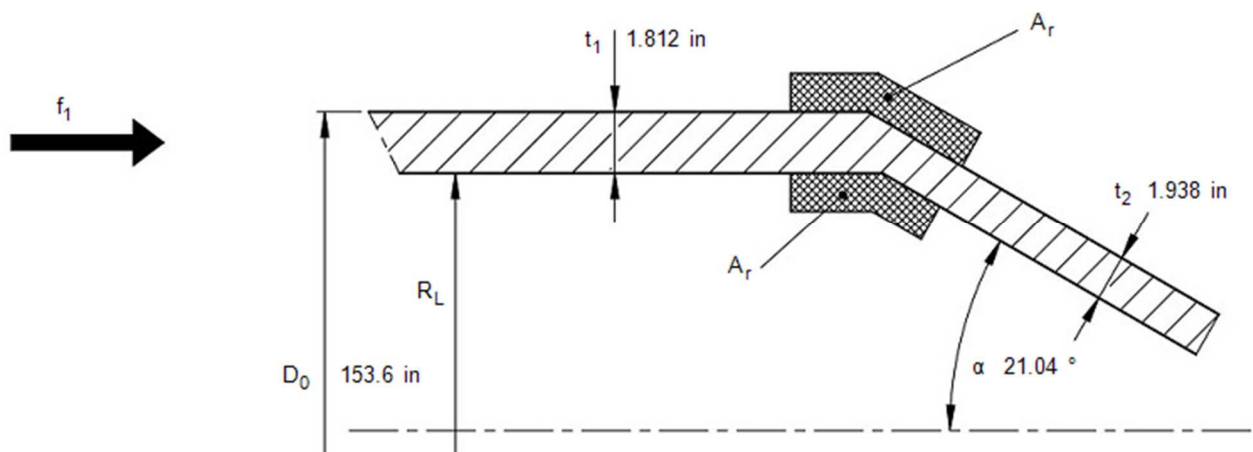
Hydrostatic head

Calculation pressure

Calculation temperature

Axial load based on circumference (for compression negative)

p_D	356 psi
D_p	0 psi
p_0	356 psi
T_0	300 °F
f_1	0 lbf/in



Cylinder

Outside diameter

Final wall thickness

Material K02700-SA-516-70-Class:-Size:

Wall thickness allowance

Allowance (corrosion)

Thickness without allowances

Inside radius

(= $D_0/2 - t_s$)

Allowable stress

Modulus of elasticity

Weld joint efficiency (or Cast Quality Factor)

D_0	153.6 in
t_1	1.812 in
c_1	0 in
c_2	0.125 in
t_s	1.687 in
R_L	75.12 in
S_s	20015 psi
E_s	2.829e+7 psi
E_1	1

Cone

Half-apex angle ($\leq 30^\circ$)

Final wall thickness

Material K02700-SA-516-70-Class:-Size:

Wall thickness allowance

Allowance (corrosion)

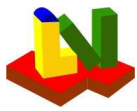
Effective thickness

Allowable stress

Modulus of elasticity

Weld joint efficiency (or Cast Quality Factor)

α	21.04 °
t_2	1.938 in
c_1	0 in
c_2	0.125 in
t_c	1.813 in
S_c	20015 psi
E_c	2.829e+7 psi
E_2	1



ASME BPVC VIII-1 2019

Example E4.3.7 - E4.3.8 PTB-4-2013

Results

Geometrical conditions

valid

Strength condition

Wall thickness acceptable

Factor			k	1
Ratio		$P_0/S_s E_1$		0.01779
Angle	(Reinforcement required if $\Delta <$	21.04	Δ	30 °
	α			
Effective load			Q_L	13371 lbf/in
Required thickness cylinder (UG-27)			t	1.351 in
with allowances (t_1)	1.812 in	$\geq t_+$	t_+	1.476 in
Required thickness cone (UG-32)			t_r	1.447 in
with allowances (t_2)	1.938 in	$\geq t_+$	t_{r+}	1.572 in
Required cross sectional area			A_{rL}	0 in ²
Available cross section			A_{eL}	8.209 in ²
Required area of reinforcement			A_r	0 in ²
Available area of reinforcement		$b_v \cdot t_v$	A_v	0 in ²
Maximum distance from the connection point of the complete reinforcing area		$\sqrt{[R_L \cdot t_s]}$		11.26 in
centroid of reinforcing area		$0.25 \cdot \sqrt{[R_L \cdot t_s]}$		2.815 in

Equations

$$\cos(\alpha) = \cos(\alpha) \Leftrightarrow \cos(21.04^\circ) = 0.9333$$

$$\tan(\alpha) = \tan(\alpha) \Leftrightarrow \tan(21.04^\circ) = 0.3846$$

$$Q_L = P_0 \cdot \frac{R_L}{2} + f_1 = 24.55 \text{ bar} \cdot \frac{1908 \text{ mm}}{2} + 0 \text{ N/mm} = 2342 \text{ N/mm}$$

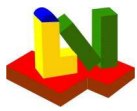
$$A_{rL} = \frac{k \cdot Q_L \cdot R_L}{S_s \cdot E_1} \cdot \left[1 - \frac{D_{el}}{\alpha} \right] \cdot \tan(\alpha) = \frac{1 \cdot 2342 \text{ N/mm} \cdot 1908 \text{ mm}}{138 \text{ N/mm}^2 \cdot 1} \cdot \left[1 - \frac{30^\circ}{21.04^\circ} \right] \cdot 0.3846 = 0 \text{ mm}^2$$

$$t = \frac{P_0 \cdot R_L}{S_s \cdot E_1 - 0.6 \cdot P_0} = \frac{24.55 \text{ bar} \cdot 1908 \text{ mm}}{138 \text{ N/mm}^2 \cdot 1 - 0.6 \cdot 24.55 \text{ bar}} = 34.3 \text{ mm}$$

$$t_r = \frac{P_0 \cdot \frac{R_L}{\cos(\alpha)}}{S_c \cdot E_2 - 0.6 \cdot P_0} = \frac{24.55 \text{ bar} \cdot \frac{1908 \text{ mm}}{0.9333}}{138 \text{ N/mm}^2 \cdot 1 - 0.6 \cdot 24.55 \text{ bar}} = 36.75 \text{ mm}$$

$$A_{eL} = (t_s - t) \cdot \sqrt{R_L \cdot t_s} + (t_c - t_r) \cdot \sqrt{R_L \cdot \frac{t_c}{\cos(\alpha)}} =$$

$$(42.86 \text{ mm} - 34.3 \text{ mm}) \cdot \sqrt{1908 \text{ mm} \cdot 42.86 \text{ mm}} + (46.04 \text{ mm} - 36.75 \text{ mm}) \cdot \sqrt{1908 \text{ mm} \cdot \frac{46.04 \text{ mm}}{0.9333}} = 5296 \text{ mm}^2$$



E4.3.7 Small End - Cone-to-cylinder junction at small end under internal pressure - ASME BPVC VIII-1 UG-32 & Appendix-1: 2019

Cone-to-cylinder junction (small end)

Type of reinforcing ring

(0 = no, 1 = at the cylinder, 2 = at the cone)

Without stiffener

Design pressure

Hydrostatic head

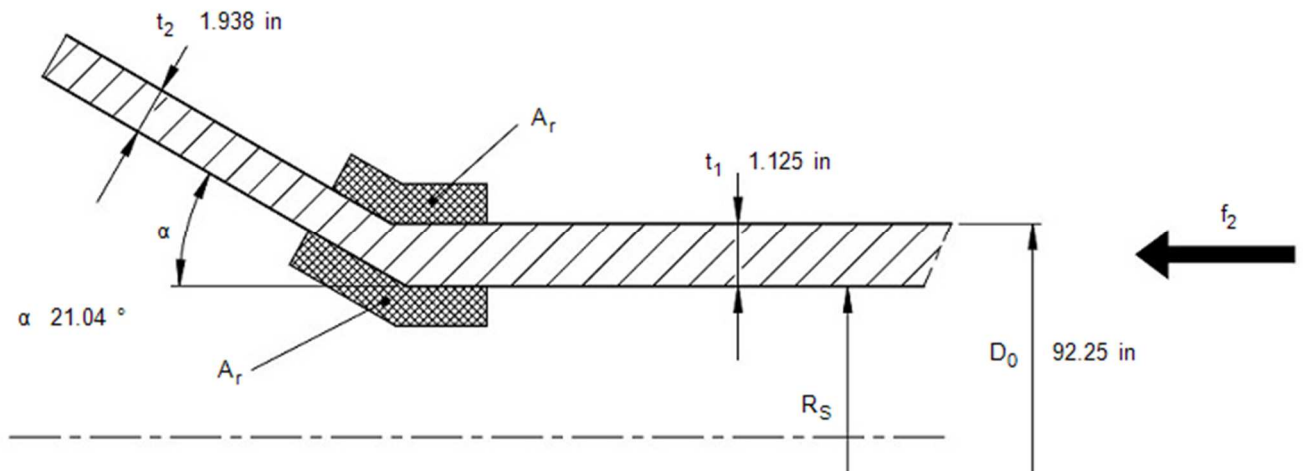
Calculation pressure

Calculation temperature

Axial load based on circumference (for compression negative)

p_D	356 psi
D_p	0 psi
p_0	356 psi
T_0	300 °F
f_2	396.9 lbf/in

0



Cylinder

Outside diameter

Final wall thickness

Material K02700-SA-516-70-Class:-Size:

Wall thickness allowance

Allowance (corrosion)

Effective thickness

Inside radius

(= $D_0/2 - t_s$)

Allowable stress

Modulus of elasticity

Weld joint efficiency (or Cast Quality Factor)

D_0	92.25 in
t_1	1.125 in
c_1	0 in
c_2	0.125 in
t_s	1 in
R_s	45.12 in
S_s	20015 psi
E_s	2.829e+7 psi
E_1	1

Cone

Half-apex angle ($\leq 30^\circ$)

Final wall thickness

Material K02700-SA-516-70-Class:-Size:

Wall thickness allowance

Allowance (corrosion)

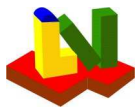
Thickness without allowances

Allowable stress

Modulus of elasticity

Weld joint efficiency (or Cast Quality Factor)

α	21.04 °
t_2	1.938 in
c_1	0 in
c_2	0.125 in
t_c	1.813 in
S_c	20015 psi
E_c	2.829e+7 psi
E_2	1



ASME BPVC VIII-1 2019

Example E4.3.7 - E4.3.8 PTB-4-2013

Results

Geometrical conditions

valid

Strength condition

Wall thickness acceptable

Factor			k	1
Ratio	$P_0/S_s E_1$		Δ	0.01779
Angle			Q_s	11.73 °
Effective load				8429 lbf/in
Required thickness cylinder (UG-27)			t	0.8113 in
with allowances (t_1)	1.125 in	$\geq t_+$	t_+	0.9363 in
Required thickness cone (UG-32)			t_r	0.8692 in
with allowances (t_2)	1.938 in	$\geq t_r$	t_r	0.9942 in
Required cross sectional area			A_{rS}	3.235 in ²
Available cross section			A_{eS}	6.284 in ²
Required area of reinforcement			A_r	0 in ²
Available area of reinforcement	$b_v \cdot t_v$		A_v	0 in ²
Maximum distance from the connection point of the complete reinforcing area	$\sqrt{[R_L \cdot t_s]}$			9.044 in
centroid of reinforcing area	$0.25 \cdot \sqrt{[R_L \cdot t_s]}$			2.261 in

Equations

$$\cos(\alpha) = \cos(\alpha) \Leftrightarrow \cos(21.04^\circ) = 0.9333$$

$$\tan(\alpha) = \tan(\alpha) \Leftrightarrow \tan(21.04^\circ) = 0.3846$$

$$QS = P_0 \cdot \frac{RS}{2} + f_2 = 24.55 \text{ bar} \cdot \frac{1146 \text{ mm}}{2} + 69.5 \text{ N/mm} = 1476 \text{ N/mm}$$

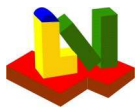
$$ArS = \frac{k \cdot QS \cdot RS}{SS \cdot E_1} \cdot \left[1 - \frac{Del}{\alpha} \right] \cdot \tan(\alpha) = \frac{1 \cdot 1476 \text{ N/mm} \cdot 1146 \text{ mm}}{138 \text{ N/mm}^2 \cdot 1} \cdot \left[1 - \frac{11.73^\circ}{21.04^\circ} \right] \cdot 0.3846 = 2087 \text{ mm}^2$$

$$t = \frac{P_0 \cdot RS}{S_s \cdot E_1 - 0.6 \cdot P_0} = \frac{24.55 \text{ bar} \cdot 1146 \text{ mm}}{138 \text{ N/mm}^2 \cdot 1 - 0.6 \cdot 24.55 \text{ bar}} = 20.61 \text{ mm}$$

$$tr = \frac{P_0 \cdot \frac{RS}{(\cos(\alpha))}}{S_c \cdot E_2 - 0.6 \cdot P_0} = \frac{24.55 \text{ bar} \cdot \frac{1146 \text{ mm}}{0.9333}}{138 \text{ N/mm}^2 \cdot 1 - 0.6 \cdot 24.55 \text{ bar}} = 22.08 \text{ mm}$$

$$AeS = 0.78 \cdot \sqrt{RS \cdot ts} \cdot \left[(ts - t) + \frac{(tc - tr)}{\cos(\alpha)} \right] =$$

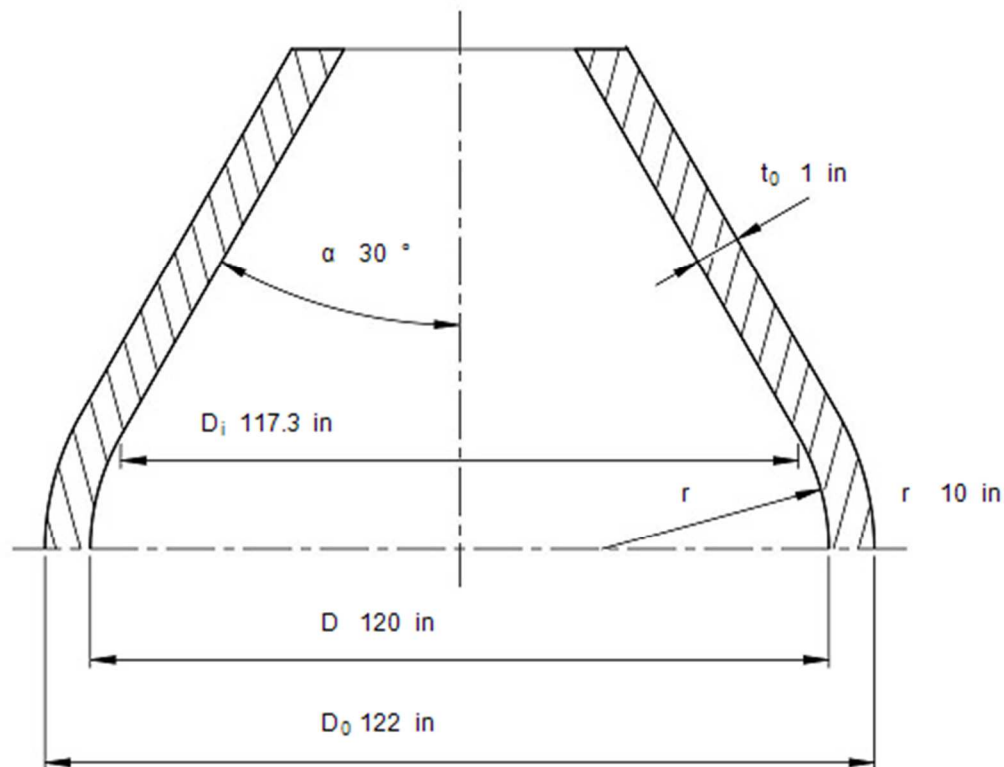
$$0.78 \cdot \sqrt{1146 \text{ mm} \cdot 25.4 \text{ mm}} \cdot \left[(25.4 \text{ mm} - 20.61 \text{ mm}) + \frac{(46.04 \text{ mm} - 22.08 \text{ mm})}{0.9333} \right] = 4054 \text{ mm}^2$$



E4.3.8 - Cone with knuckle under internal pressure - ASME BPVC VIII-1 UG-32 & Appendix-1: 2019

Toriconical sections

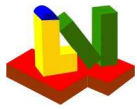
Design pressure	p_D	285.4 psi
Hydrostatic head	D_p	0 psi
Calculation pressure	p_0	285.4 psi
Calculation temperature	T_0	300 °F
Final wall thickness	t_e	1 in
Wall thickness allowance	c_1	0 in
Allowance (corrosion)	c_2	0 in
Effective thickness without allowances	t_0	1 in



Outside diameter of cylindrical shell	D_0	122 in
Inside diameter of cylindrical shell	D	120 in
Semi-apex angle	α	30 °
Knuckle radius ($\geq 0.06 \cdot D_0, \geq 3 \cdot t_e$)	r	10 in
Weld joint efficiency (or Cast Quality Factor)	E	1

Material K02700-SA-516-70-Class:-Size:

Allowable stress S **20015** psi



ASME BPVC VIII-1 2019

Example E4.3.7 - E4.3.8 PTB-4-2013

Calculation

Largest inside diameter of cone	D_i	117.3 in
Equivalent radius	L	67.74 in
Ratio	L/r	6.774
Factor	M	1.401
Required knuckle thickness	t	0.6773 in
Allowable inside pressure of knuckle	P	421 psi

Calculation diameter of cone	D_1	117.3 in
Required cone thickness at D_1	t_1	0.9741 in
Allowable inside pressure of cone	P_1	292.9 psi

Remark

Required thickness incl. allowances	$t+C_1+C_2$	$t+$	0.9741 in
Allowable excess pressure	$\text{Min}(P, P_1)$	P_m	292.9 psi
Allowable excess pressure without hydr. Head		MAWP	292.9 psi

Geometrical conditions

valid

Strength condition

Wall thickness acceptable

Equations knuckle

$$\cos(\alpha) = \cos(\alpha) \Leftrightarrow \cos(30^\circ) = 0.866$$

$$D_i = D - 2 \cdot r \cdot (1 - \cos(\alpha)) = 3048 \text{ mm} - 2 \cdot 254 \text{ mm} \cdot (1 - 0.866) = 2980 \text{ mm}$$

$$L = \frac{D_i}{2 \cdot \cos(\alpha)} = \frac{2980 \text{ mm}}{2 \cdot 0.866} = 1720 \text{ mm}$$

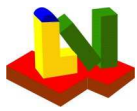
$$t = \frac{P_0 \cdot L \cdot M}{2 \cdot S \cdot E - 0.2 \cdot P_0} = \frac{19.68 \text{ bar} \cdot 1720 \text{ mm} \cdot 1.401}{2 \cdot 138 \text{ N/mm}^2 \cdot 1 - 0.2 \cdot 19.68 \text{ bar}} = 17.2 \text{ mm}$$

$$P = \frac{2 \cdot S \cdot E \cdot t_0}{L \cdot M + 0.2 \cdot t_0} = \frac{2 \cdot 138 \text{ N/mm}^2 \cdot 1 \cdot 25.4 \text{ mm}}{1720 \text{ mm} \cdot 1.401 + 0.2 \cdot 25.4 \text{ mm}} = 2.903 \text{ MPa}$$

Equations cone

$$t_1 = \frac{P_0 \cdot D_1}{2 \cdot \cos(\alpha) \cdot (S \cdot E - 0.6 \cdot P_0)} = \frac{19.68 \text{ bar} \cdot 2980 \text{ mm}}{2 \cdot 0.866 \cdot (138 \text{ N/mm}^2 \cdot 1 - 0.6 \cdot 19.68 \text{ bar})} = 24.74 \text{ mm}$$

$$P = \frac{2 \cdot S \cdot E \cdot t_0 \cdot \cos(\alpha)}{D_1 + 1.2 \cdot t_0 \cdot \cos(\alpha)} = \frac{2 \cdot 138 \text{ N/mm}^2 \cdot 1 \cdot 25.4 \text{ mm} \cdot 0.866}{2980 \text{ mm} + 1.2 \cdot 25.4 \text{ mm} \cdot 0.866} = 2.019 \text{ MPa}$$



ASME BPVC VIII-1 2019

Example E4.3.7 - E4.3.8 PTB-4-2013

Appendix: Material documentation

Section 2: Kegel/E4.3.7 Large End
 Section 3: Zylinder/E4.3.7 Small End
 Section 3: Kegel/E4.3.7 Small End
 Section 4: Boden/E4.3.8

Material specification:

Material code: K02700-SA-516-70-Class:-Size:	Regulation: ASME II.D Table 1A:2017	Spec. No.: SA-516
Short name: Carbon steel	Product: Plate	
Delivery condition:		

Design conditions and dimensions:

Temperature [°C]: 148.89	Thickness [mm]: 49.21
Pressure [bar]:	Outside diameter [mm]: 3901.76

Material values for test and design conditions:

	Test condition	Operating condition
Nominal design strength [N/mm²]:	138	138
Safety factor:	1	1
Allowable stress [N/mm²]:	138	138
Modulus of elasticity [kN/mm²]:	202.4	195.1

Notes:

G10: General Requirements

Upon prolonged exposure to temperatures above 425°C, the carbide phase of carbon steel may be converted to graphite. See Nonmandatory Appendix A, A-201 and A-202.

S1: Size Requirements

For Section I applications, stress values at temperatures of 450°C and above are permissible but, except for tubular products 75 mm O.D. or less enclosed within the boiler setting, use of these materials at these temperatures is not current practice.

T2: Time-Dependent Properties

Allowable stresses for temperatures of 400°C and above are values obtained from time-dependent properties.

Strength values at 20°C

R _{eH}	density	Tensile strength
.	.	R _{m, min}
N/mm²	kg/dm³	N/mm²
260	7.85	485

Strength values as a function of temperature

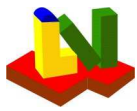
T	°C	40	100	150	250	325	375	425	475	525
K	N/mm²	138	138	138	138	132	123	83.8	51	21.3

Young's modulus-values in dependence of the temperature

T	°C	-200	-125	-75	25	100	150	200	250	300	350	400	450	500	550
E	kN/mm²	216	212	209	202	198	195	192	189	185	179	171	162	151	137

Mean coefficient of thermal expansion-values in dependence of the temperature

T	°C	20	100	200	300	400	500	600	700	800
α _m	1e-6/K	11.5	12.1	12.7	13.3	13.8	14.4	14.8	15.1	15.4



ASME BPVC VIII-1 2019
Example E4.3.7 - E4.3.8 PTB-4-2013

Differential coefficient of thermal expansion-values in dependence of the temperature

T	°C	20	100	200	300	400	500	600	700	800
α_{diff}	1e-6/K	11.5	12.7	13.8	14.9	15.9	16.7	17.0	17.1	17.7

Design conditions and dimensions:

Temperature [°C]: 148.89	Thickness [mm]: 28.58
Pressure [bar]:	Outside diameter [mm]: 2343.15

Design conditions and dimensions:

Temperature [°C]: 148.89	Thickness [mm]: 25.4
Pressure [bar]:	Outside diameter [mm]: 3098.8